

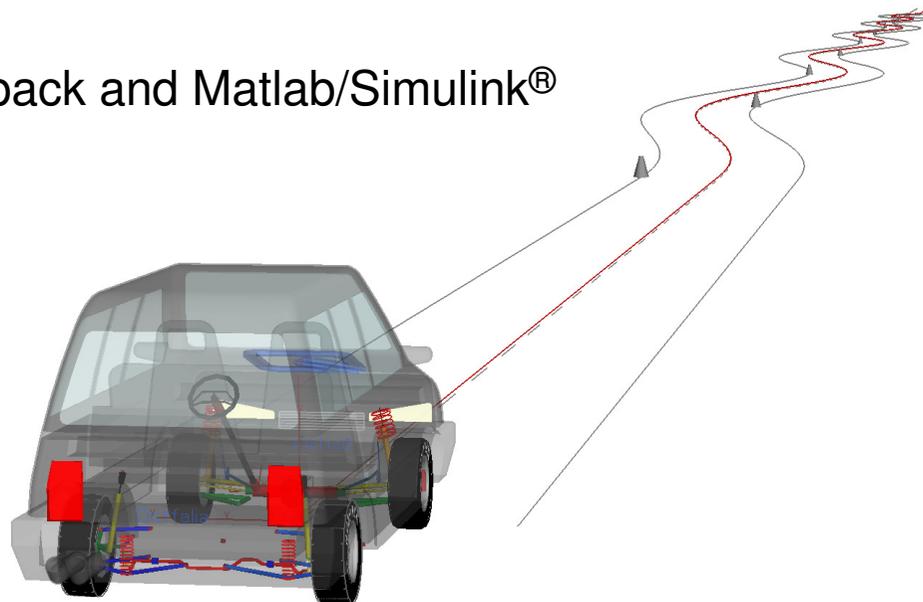
SIMPACK User Meeting 2014
October 8 – 9, Augsburg, Germany

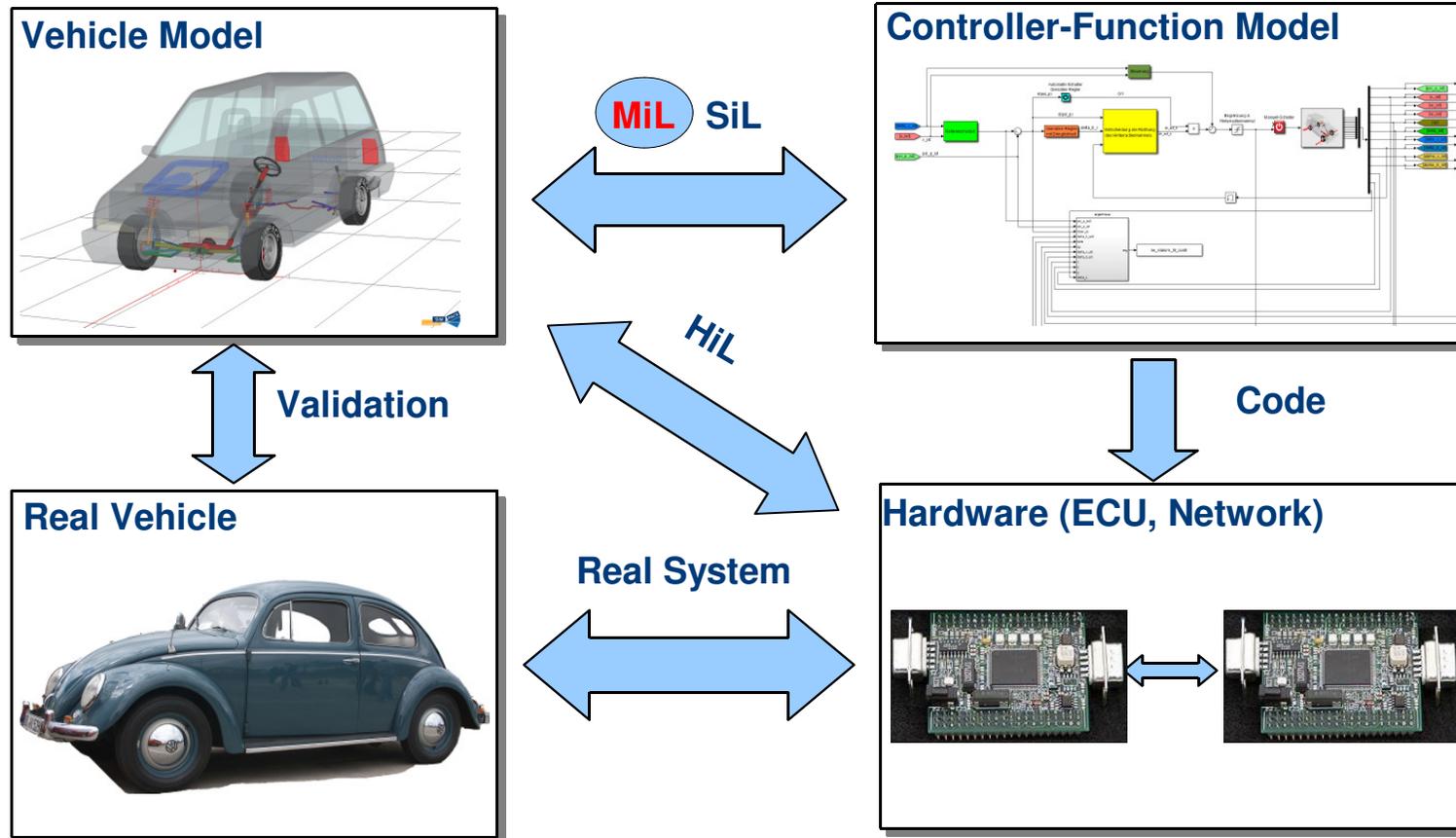
Simulation of Vehicle Dynamics Control by active Steering Systems

Volker Dorsch, Faculty of Mechanical Engineering



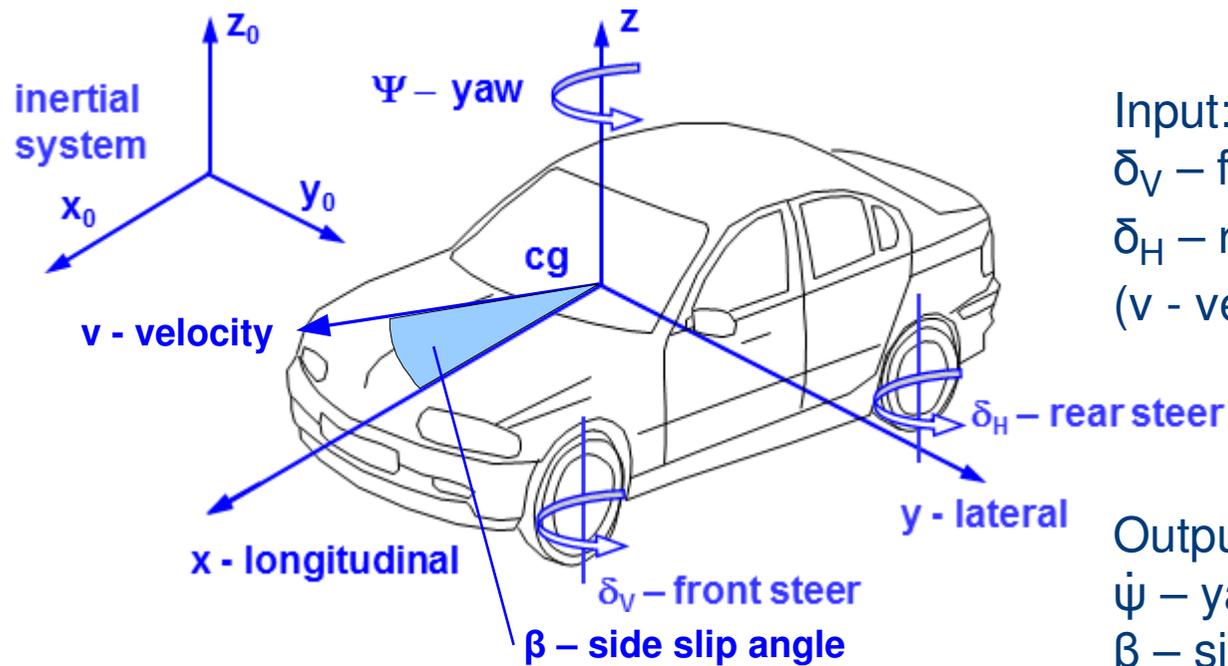
- Development scenario
- Validated mechanical multibody simulation (MBS) vehicle model
- Implementation of active steering at rear and front wheels
- Control strategy
- Co-Simulation of Simpack and Matlab/Simulink®
- Simulation Results
- Conclusions





MBS Model: Coordinates

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Input:

δ_V – front steering angle
 δ_H – rear steering angle
(v - velocity)

Output:

$\dot{\psi}$ – yaw rate
 β – side slip angle
 a_y – lateral acceleration

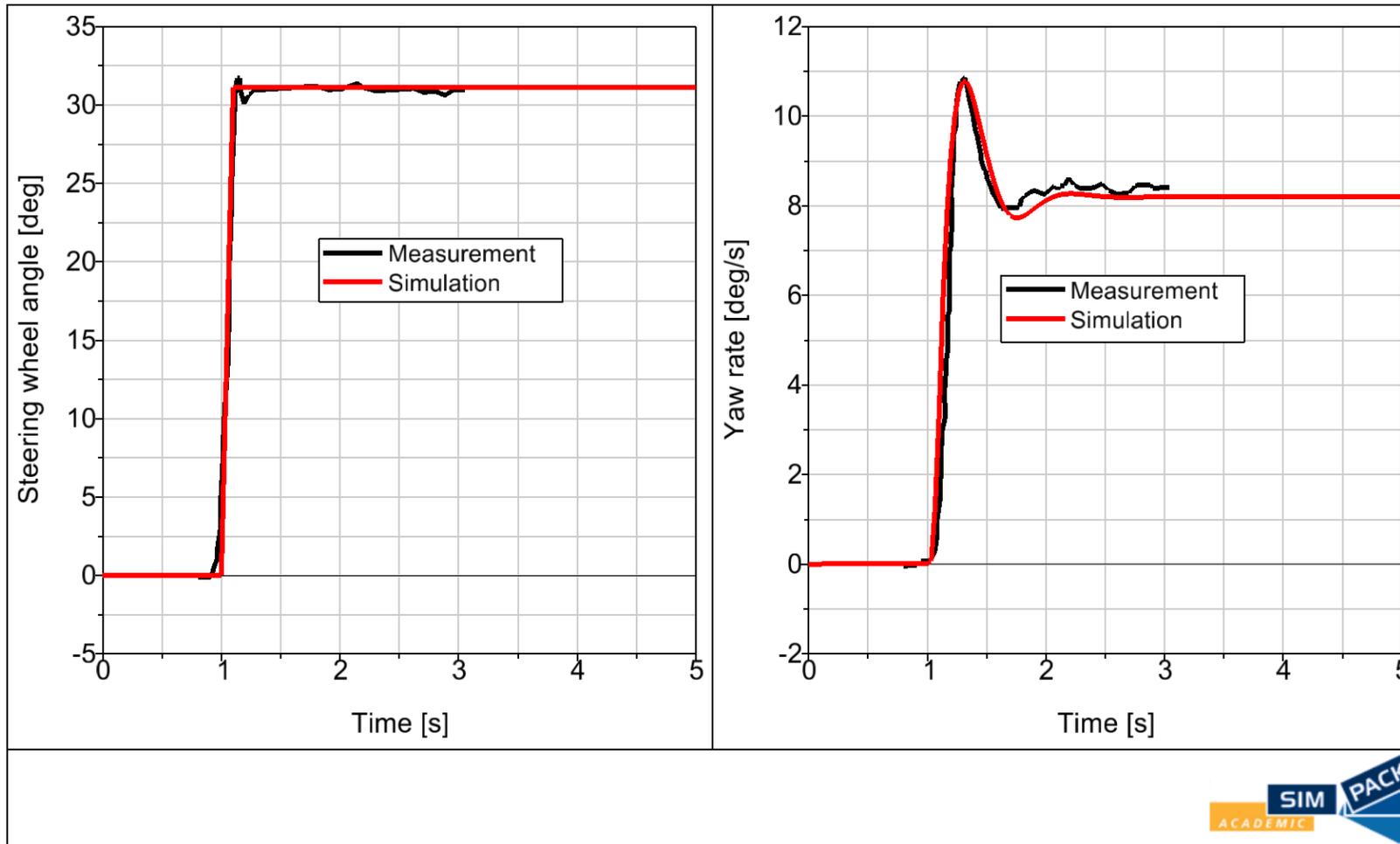
Suspensions: simulation of Kinematics and Compliance (K&C) measurements

Complete vehicle model: step steering input maneuver

driver	objective, no driver influence
velocity	100 km/h
front wheel steering angle	sudden steering angle with more than 200 deg/s steady-state lateral acceleration is 0.4 g
road surface	dry, $\mu = 0.9$

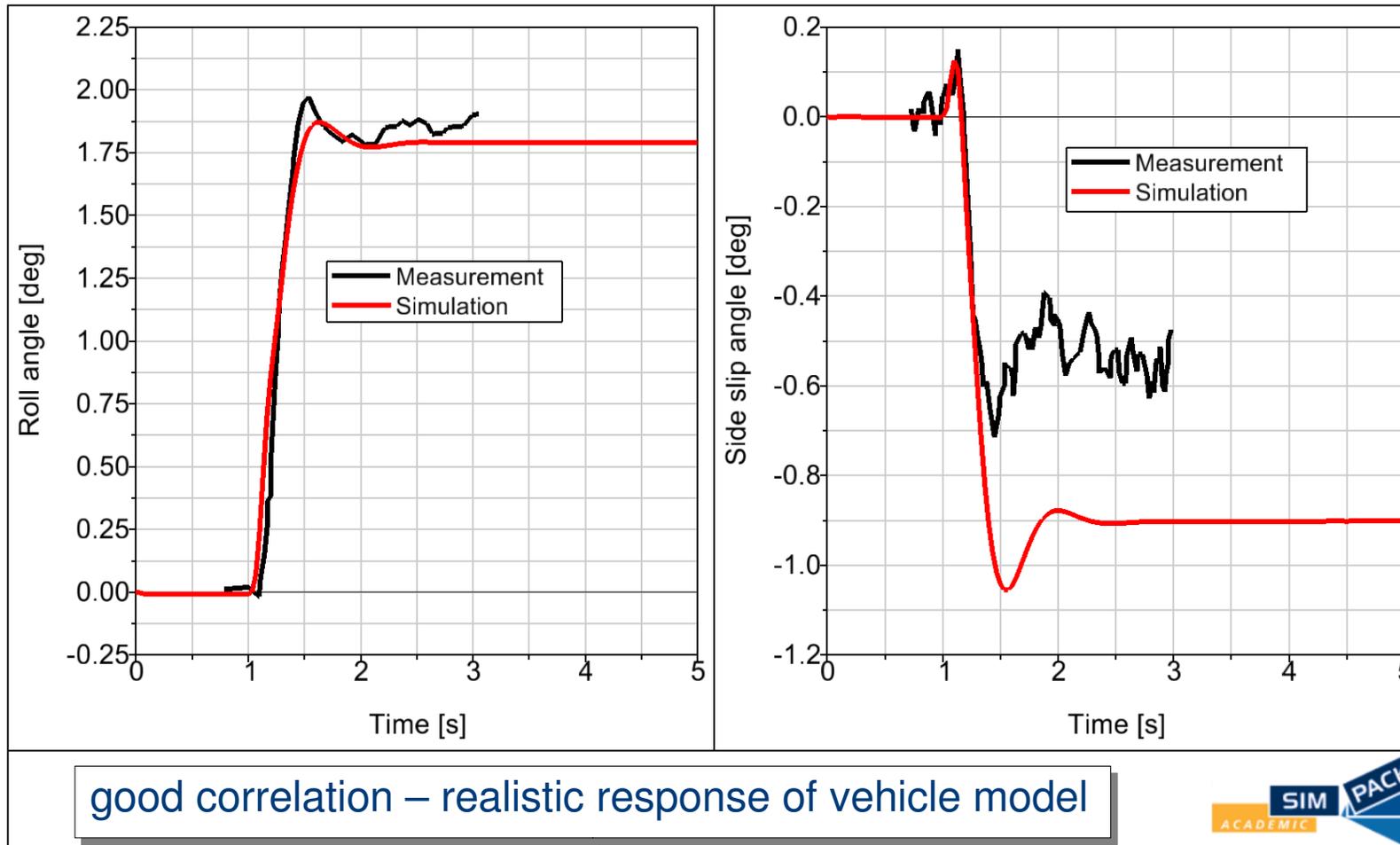
Simpack model validation: Step Steering Input

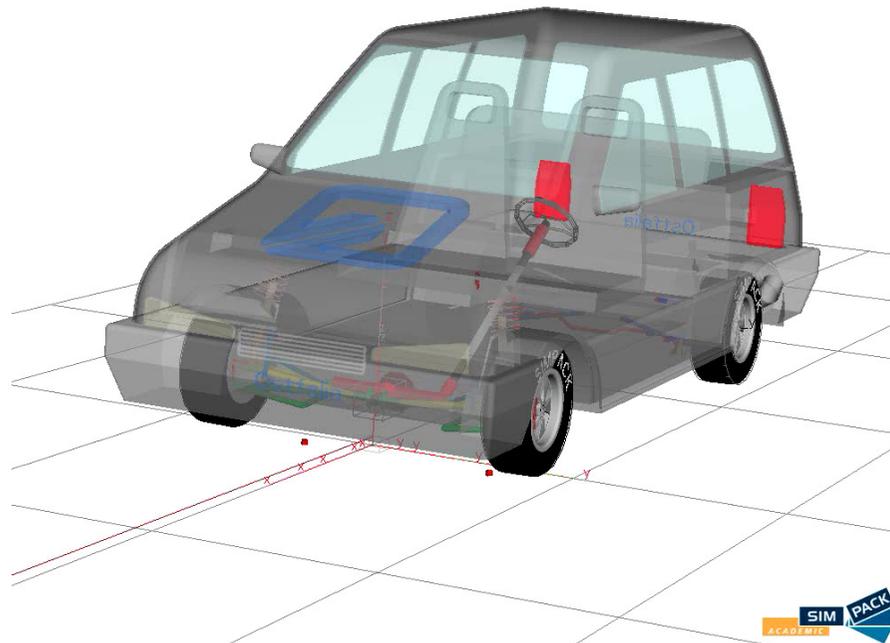
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Simpack model validation: Step Steering Input

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Active front and rear
wheel steering

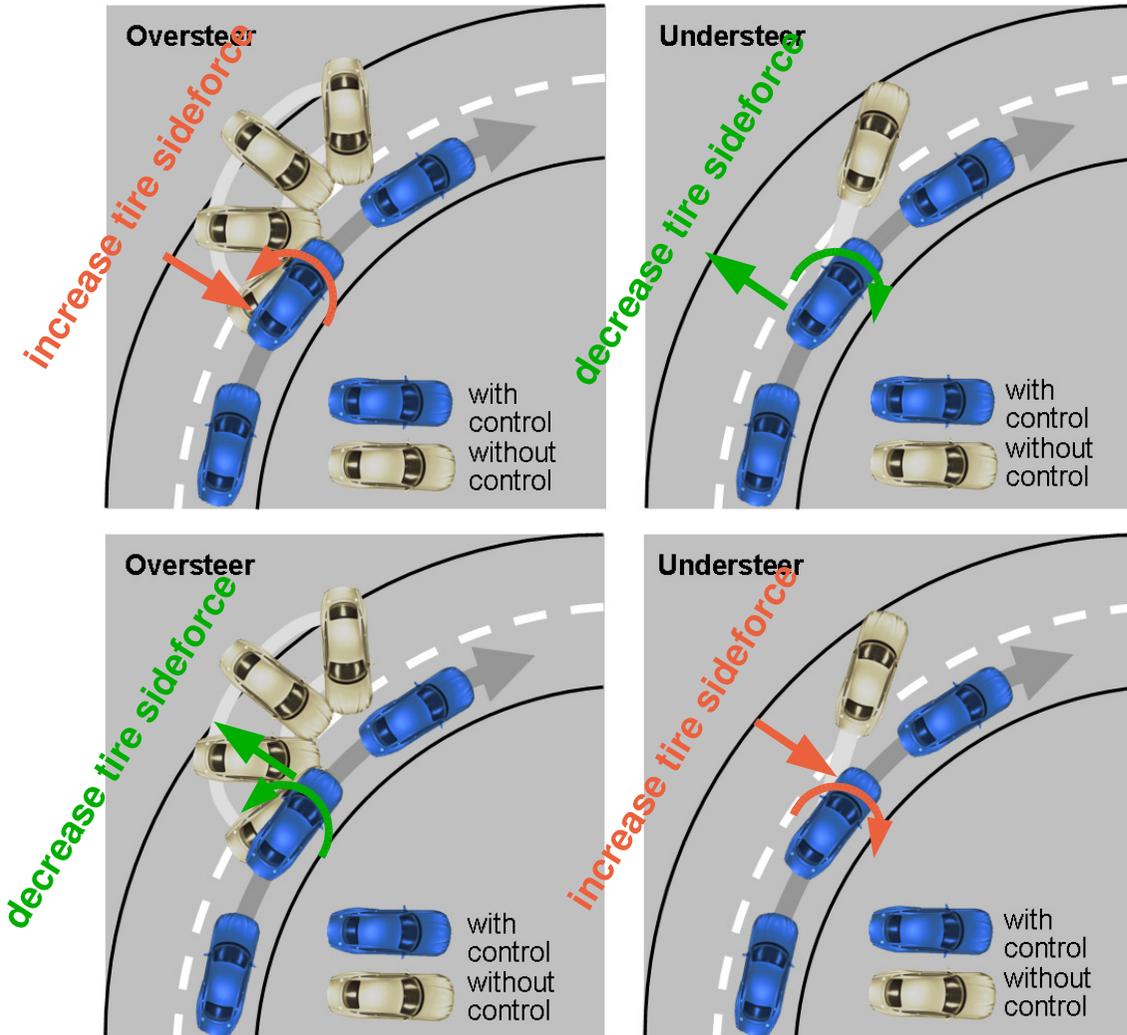
Simple implementation by

- additional rotational degrees of freedom at the corresponding wheels
- control of these degrees of freedom by external input of the co-simulated Matlab/Simulink controller model

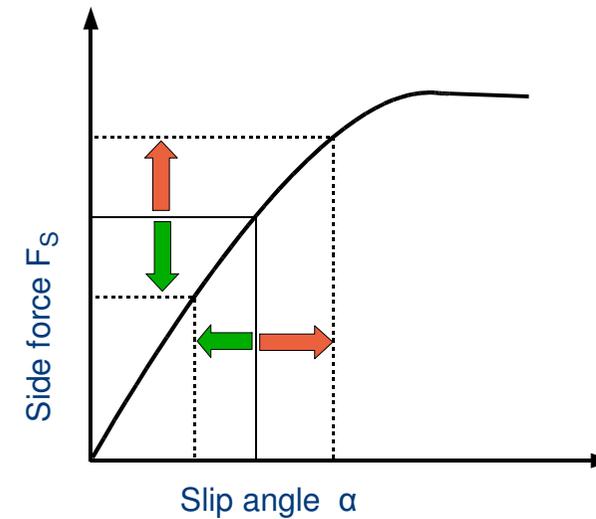
Study of effects on vehicle dynamics

Vehicle stabilization by adjusted steering angles

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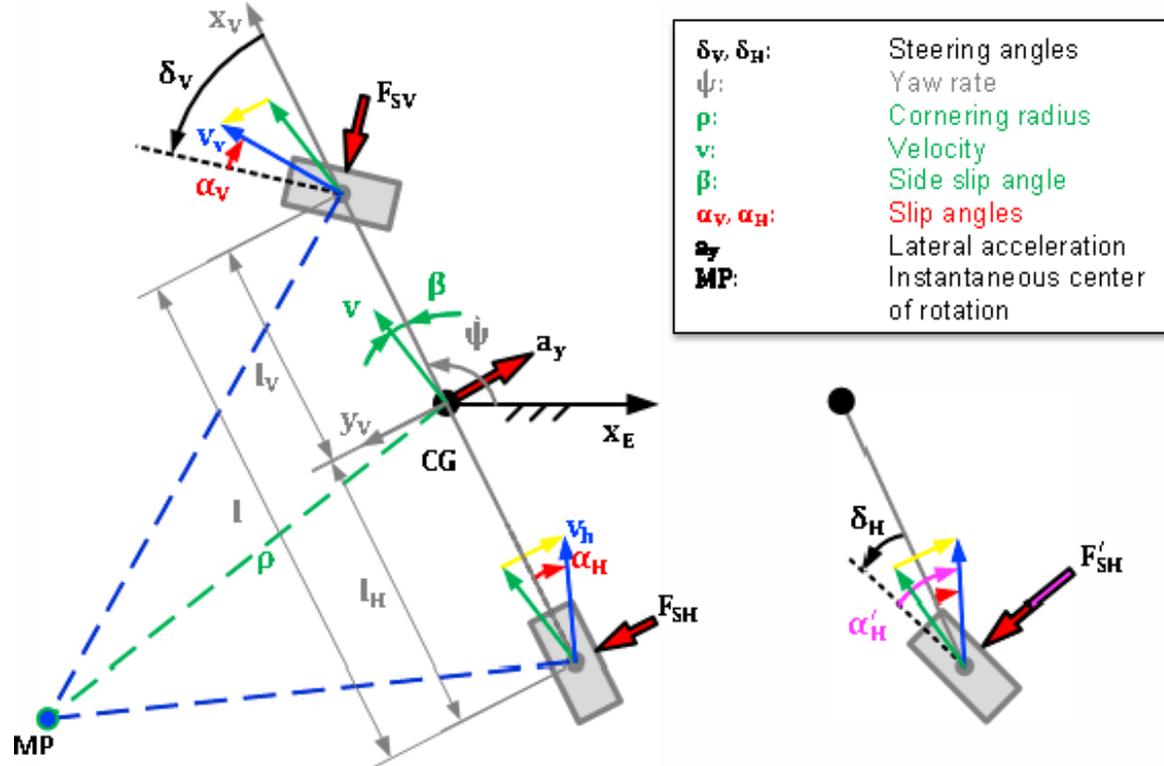
Active rear wheel steering:
adjust tire slip angle α by rear
wheel steering angle



Active front wheel steering:
adjust tire slip angle α by
superimposed steering angle

Control algorithm: bicycle model

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Equations of motion with linearized tire behavior: $F_S = C_\alpha \alpha$

$$\ddot{\psi} = \frac{C_{\alpha H} l_H - C_{\alpha V} l_V}{J_z} \beta - \frac{C_{\alpha H} l_H^2 + C_{\alpha V} l_V^2}{J_z v} \dot{\psi} + \frac{C_{\alpha V} l_V}{J_z} \delta_V - \frac{C_{\alpha H} l_H}{J_z} \delta_H$$

$$\dot{\beta} = -\frac{C_{\alpha V} + C_{\alpha H}}{m v} \beta + \left[\frac{C_{\alpha H} l_H - C_{\alpha V} l_V}{m v^2} - 1 \right] \dot{\psi} + \frac{C_{\alpha V}}{m v} \delta_V + \frac{C_{\alpha H}}{m v} \delta_H$$

In case of steady-state cornering (i.e. $\dot{\Psi}=0$ and $\dot{\beta}=0$) without rear wheel angle

$$\dot{\Psi} = \frac{v_x \delta_w}{(l_V + l_H) \left(1 + \frac{v_x^2}{v_{ch}^2}\right)}$$

The characteristic velocity v_{ch} can be computed (or be identified in tests)

$$v_{ch} = \frac{C_{\alpha V} C_{\alpha H} l^2}{m(C_{\alpha H} l_H - C_{\alpha V} l_V)}$$

Furthermore the maximum yaw rate is limited

$$|\dot{\Psi}| \leq \frac{a_{y,max}}{v_x}$$

The yaw rate $\dot{\Psi}$ is used as desired yaw rate in the control algorithm.

Control algorithm: predict rear wheel steering angle

Setting $\dot{\beta}=0$ and $\beta=0$ in the differential equations of the bicycle model yields

$$\frac{\delta_H(s)}{\delta_V(s)} = K_{\delta_H} \frac{1+T_z s}{1+T_1 s} \quad \text{with} \quad K_{\delta_H} = \frac{C_{\alpha V} C_{\alpha H} l_H l - C_{\alpha V} l_V m v^2}{C_{\alpha V} C_{\alpha H} l_V l + C_{\alpha H} l_H m v^2},$$
$$T_z = \frac{J_z v}{C_{\alpha H} l_H l - l_V m v^2},$$
$$T_1 = \frac{J_z v}{C_{\alpha V} l_V l - l_H m v^2}$$

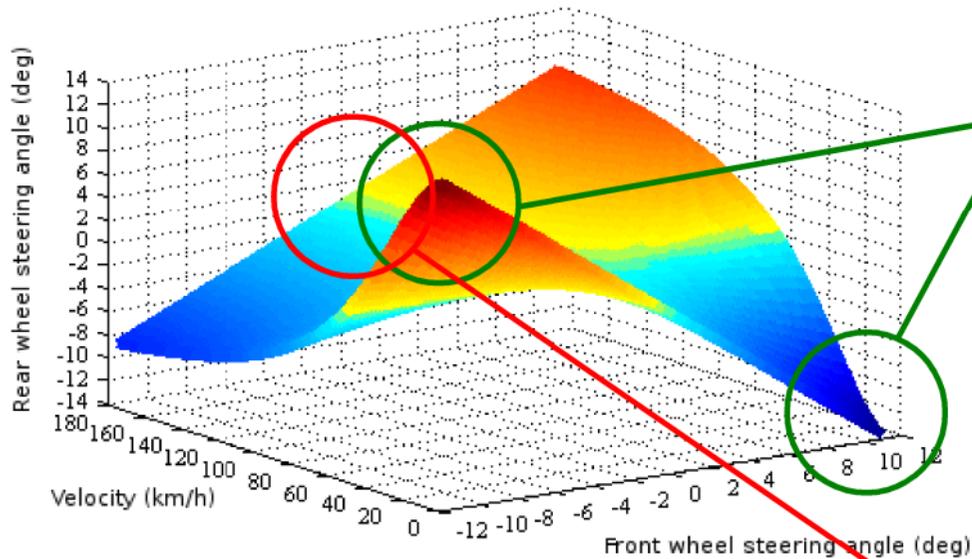
[Woernle, C.: Fahrmechanik.
Lecture notes,
University of Rostock]

The steady-state case with K_{δ_H} results in a characteristic diagram, that is used as a first prediction of the rear wheel steering angle.

Control algorithm: predict rear wheel steering angle



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low velocities and large front wheel steering angle:



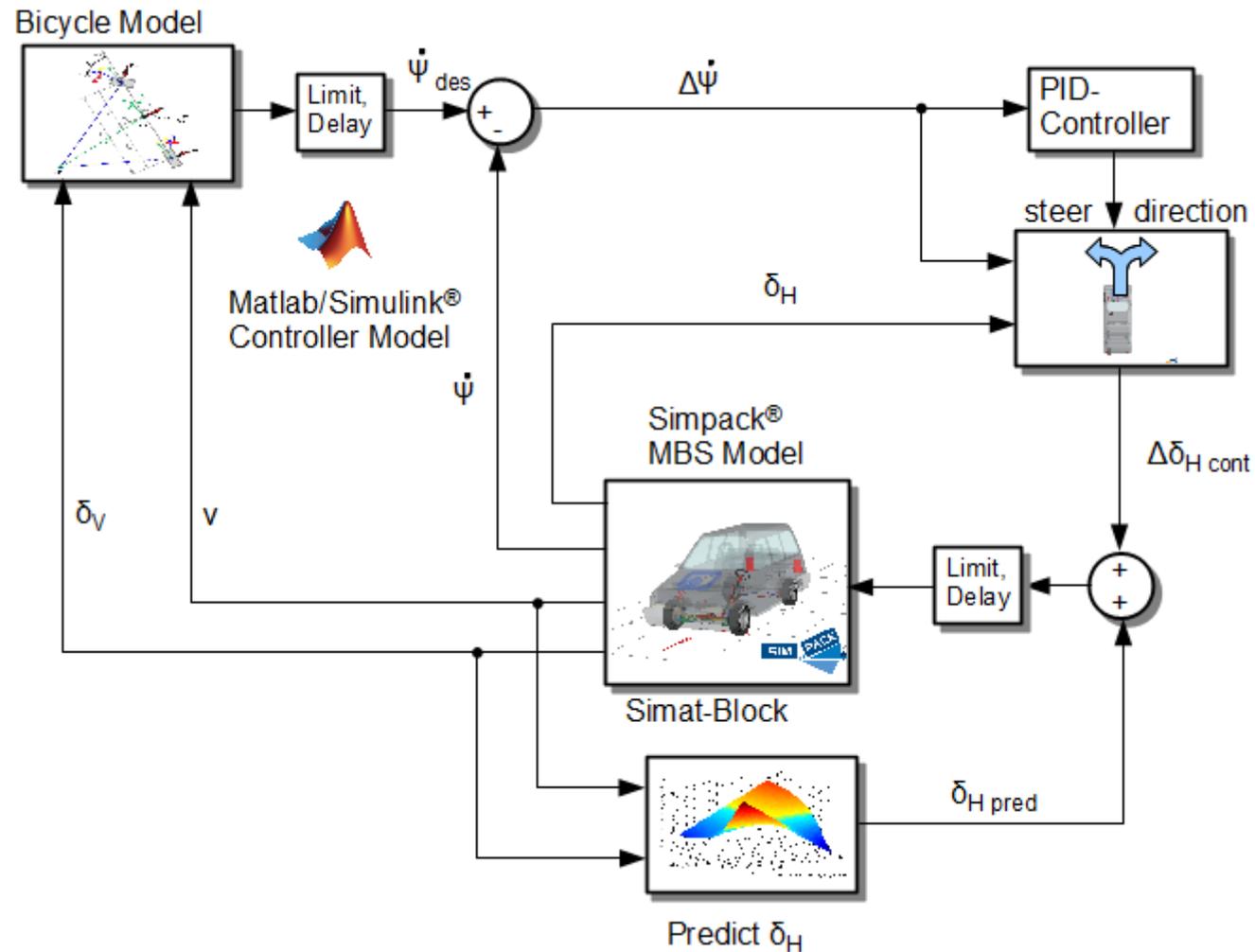
high velocities and small front wheel steering angle:



Open-loop rear wheel steering angle as predictor

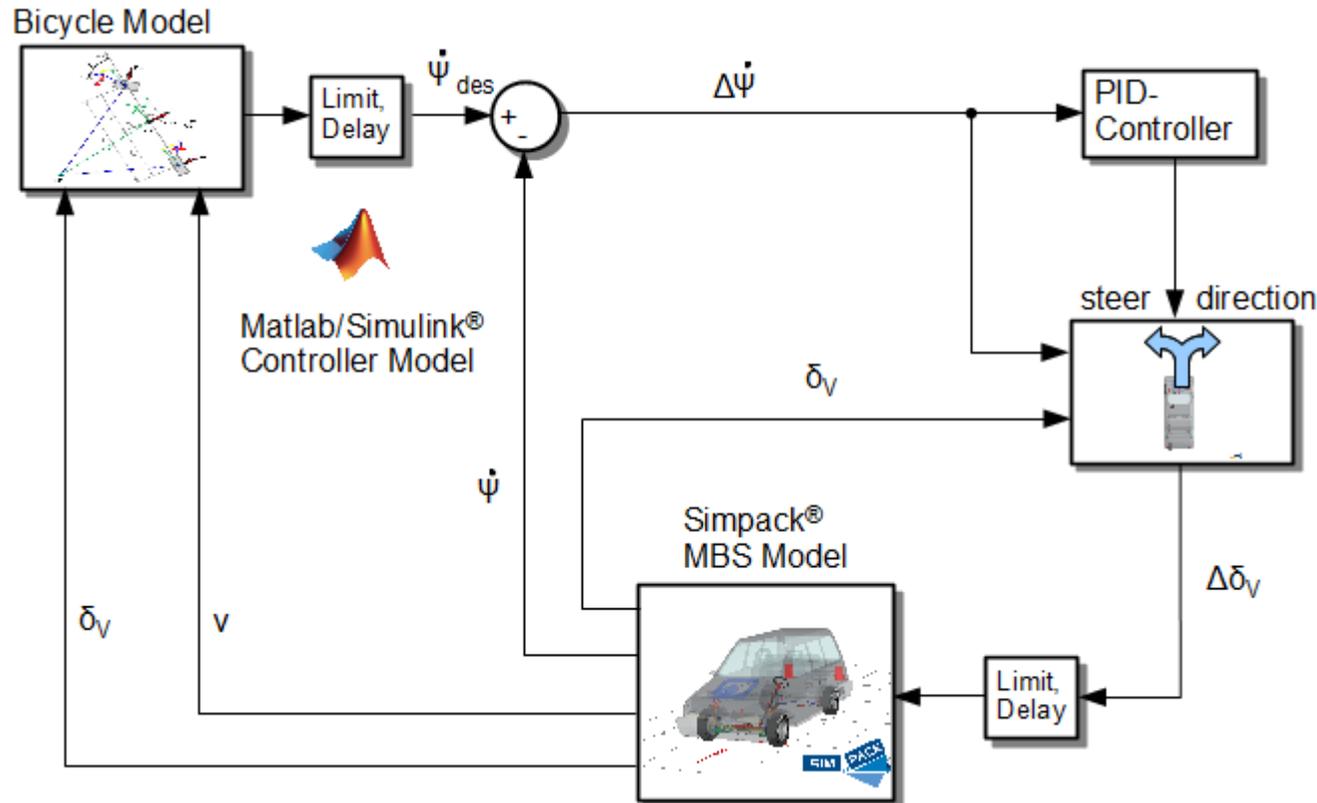
Active rear wheel steering: Control structure with co-simulation

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Active front wheel steering: Control structure with co-simulation

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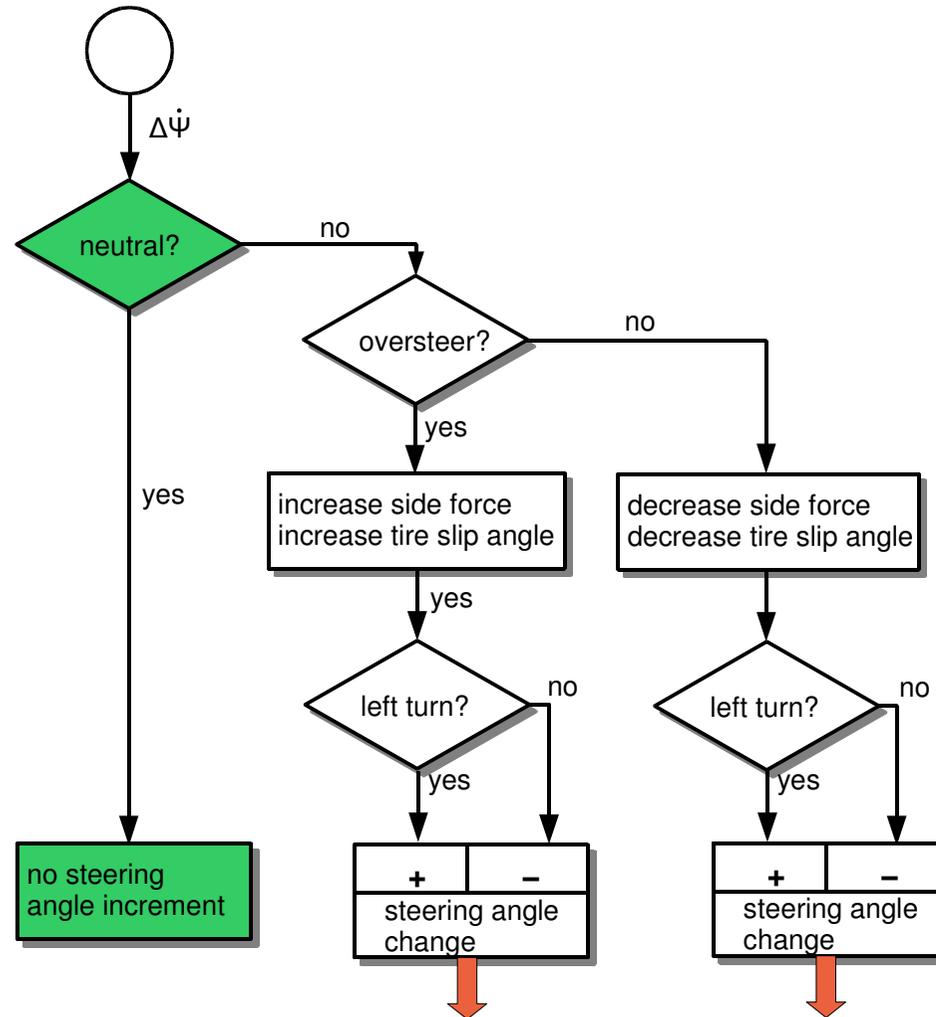
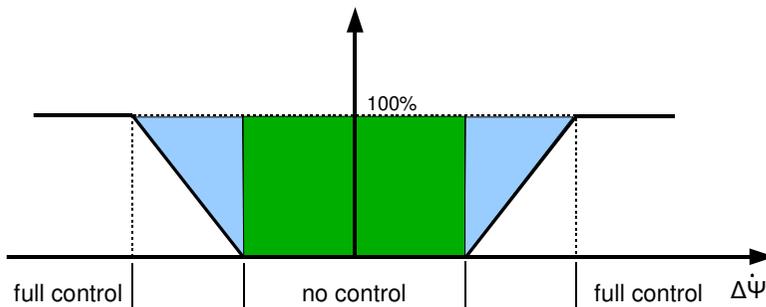


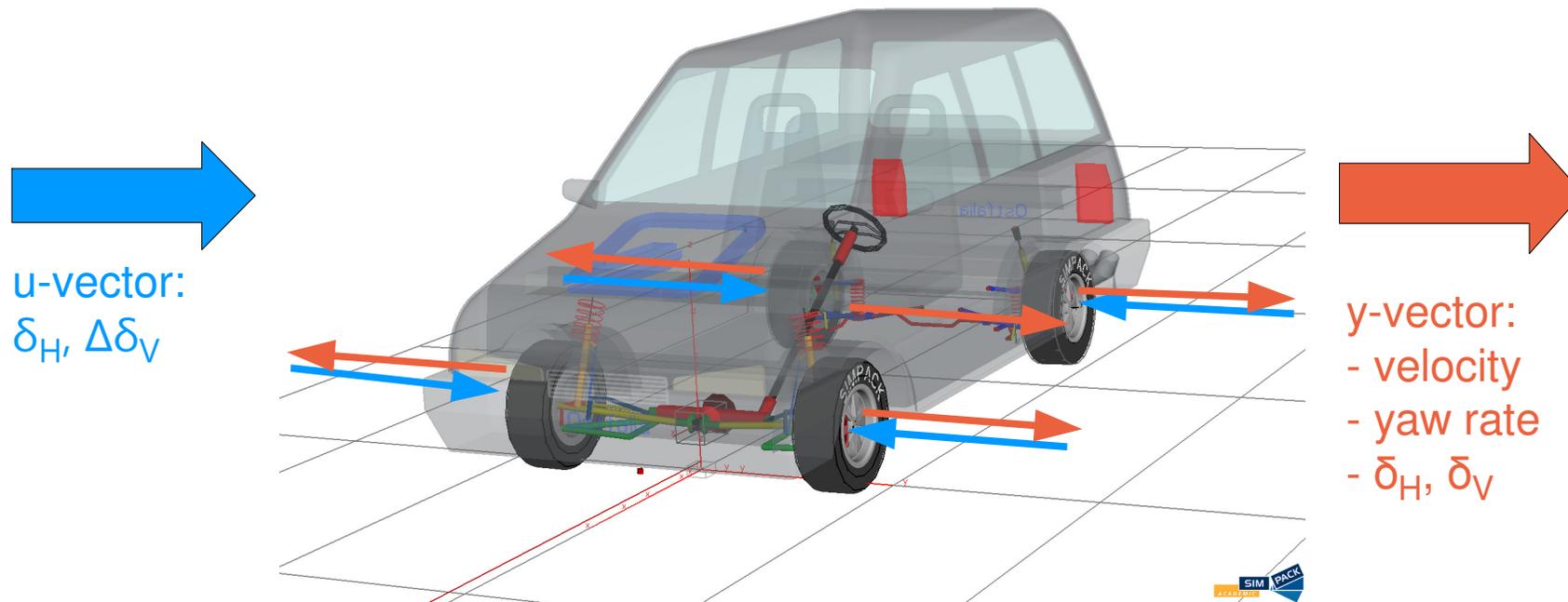
Active rear wheel steering

$|\dot{\Psi}_{des}| - |\dot{\Psi}| < 0$ oversteer
 $|\dot{\Psi}_{des}| - |\dot{\Psi}| \approx 0$ neutral
 $|\dot{\Psi}_{des}| - |\dot{\Psi}| > 0$ understeer

$\dot{\Psi} > 0$ left turn
 $\dot{\Psi} < 0$ right turn

Tolerance function to avoid hard switch on – switch off effect





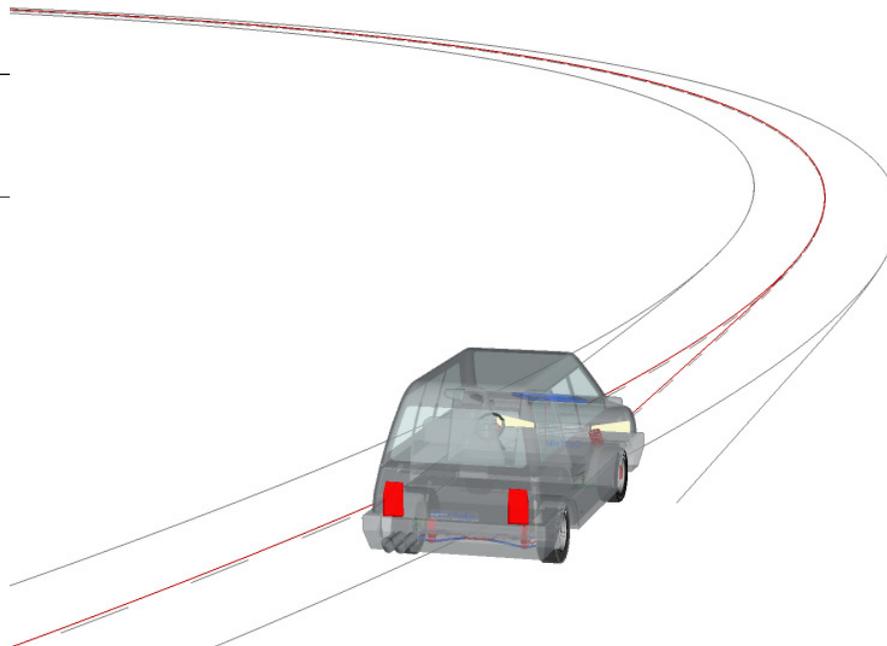
Co-simulation:

- Simpack and Matlab/Simulink® run parallel
- Data exchange at each millisecond
- Relatively slow motion of the whole vehicle: uncritical

Maneuver steady-state cornering

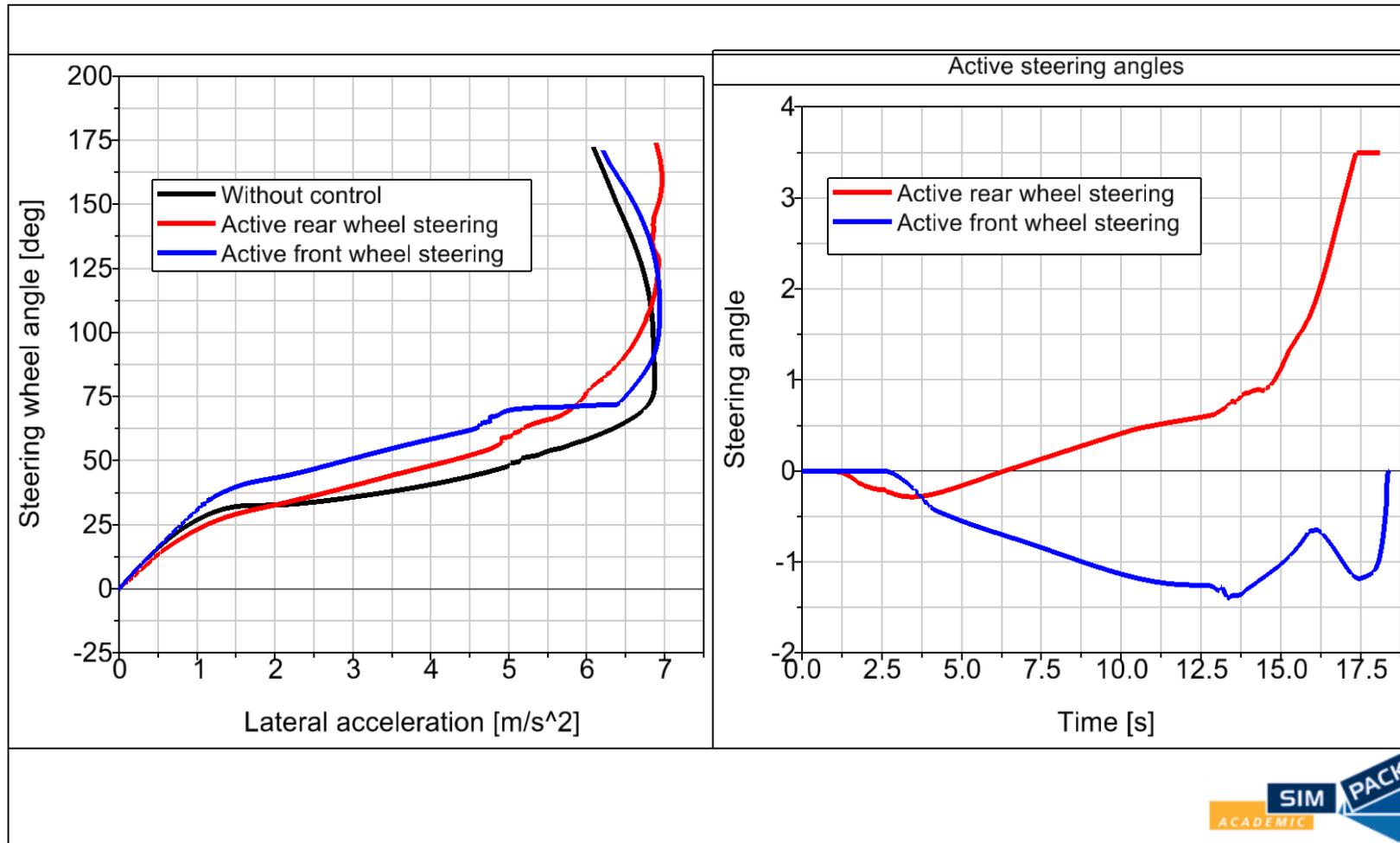
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Driver	Simpack driver model, driver influence
Velocity	increasing up to 75 km/h
Track	Circle with 80 m radius
Steering wheel angle input	closed loop, by driver
Road surface	dry, $\mu = 0.9$



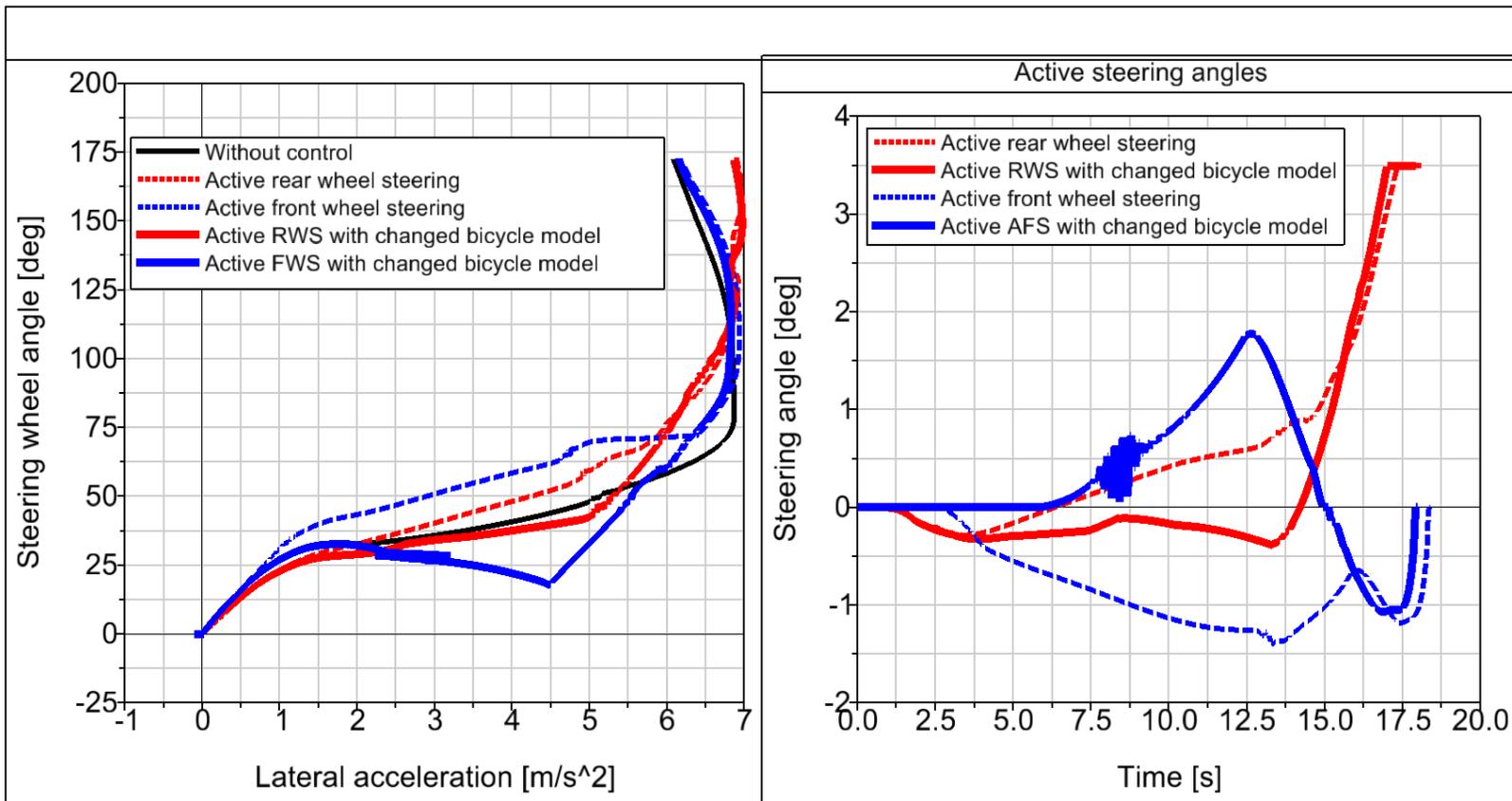
Steady-state cornering: simulation results

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Steady-state cornering: simulation results

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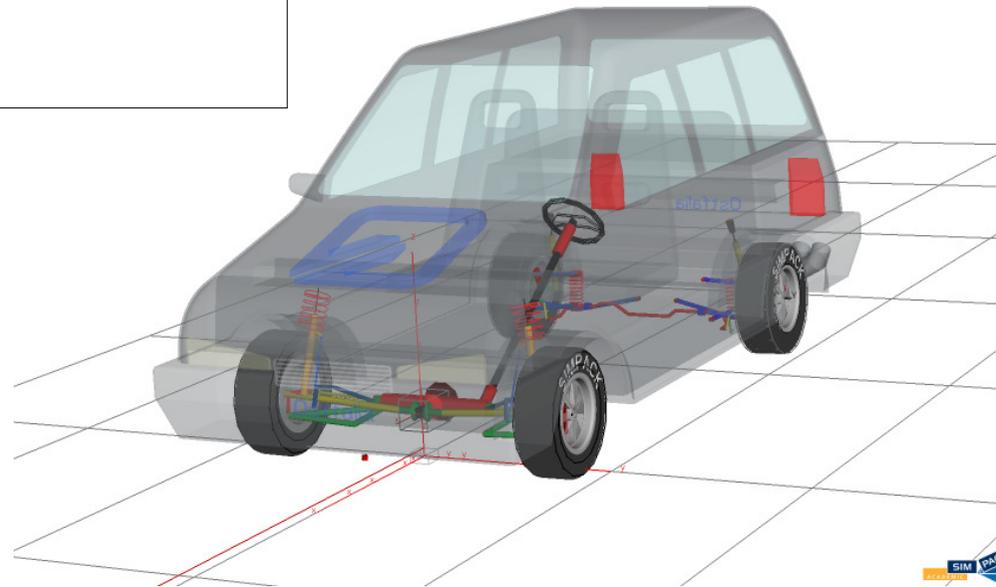
Change of cornering behavior by change of bicycle model parameters in the control algorithm



Maneuver step steering input

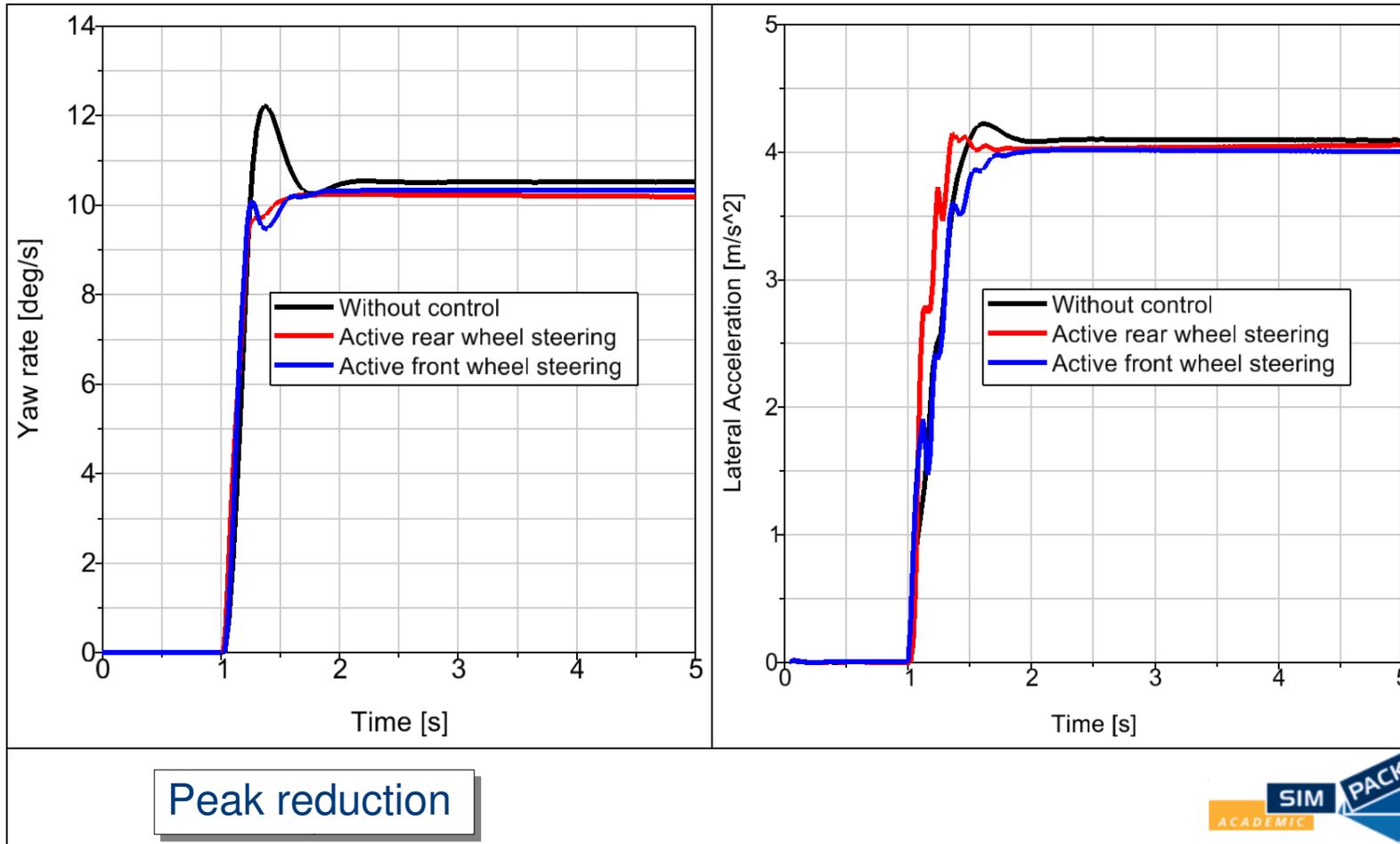
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Driver	objective, no driver influence
Velocity	80 km/h
Steering wheel angle input	sudden steering angle step with more than 200 deg/s, steady-state lateral acceleration is 0.4 g
Road surface	dry, $\mu = 0.9$



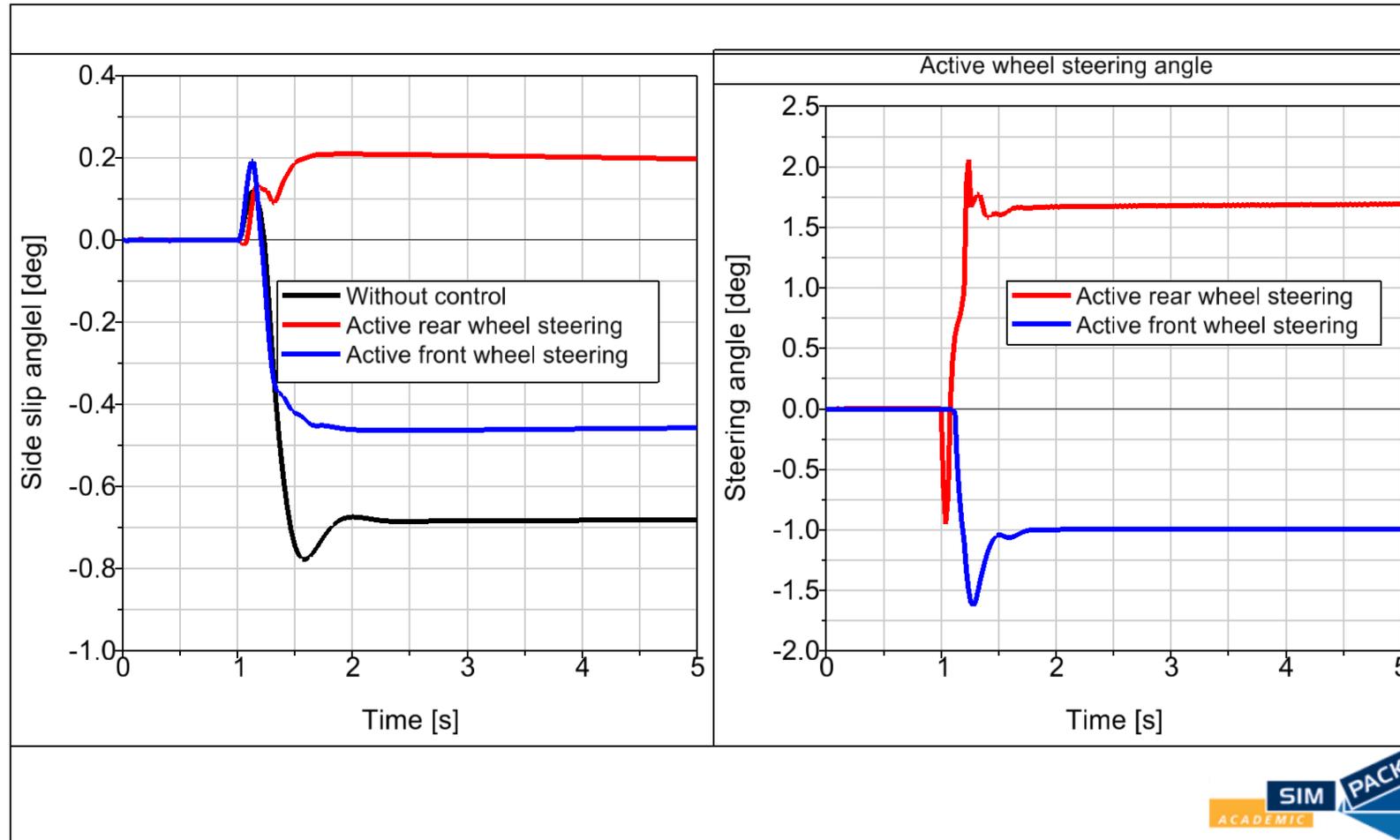
Step steering input: simulation results

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Step steering input: simulation results

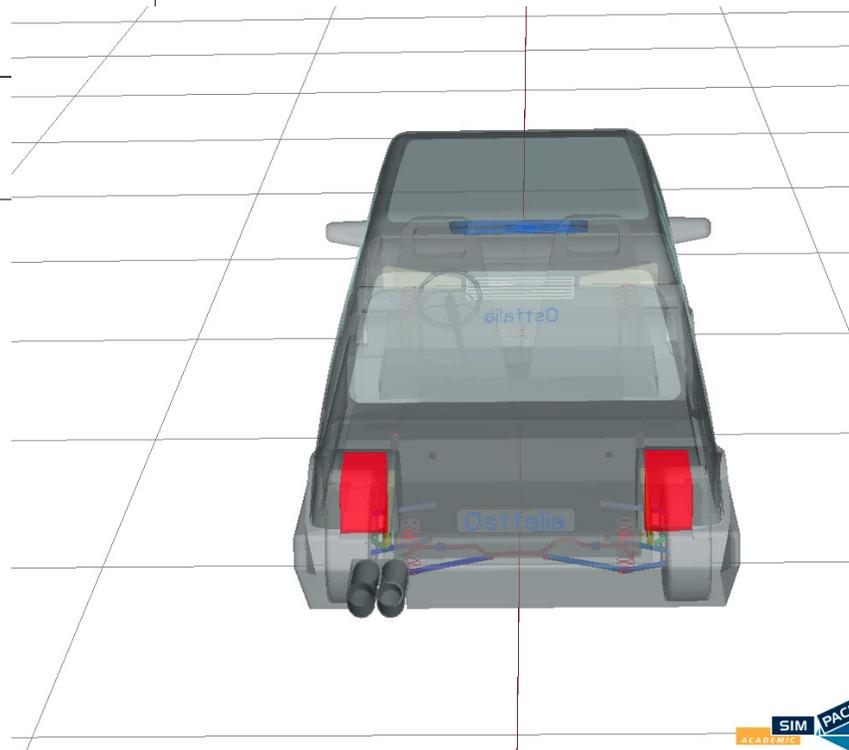
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Maneuver sine with dwell

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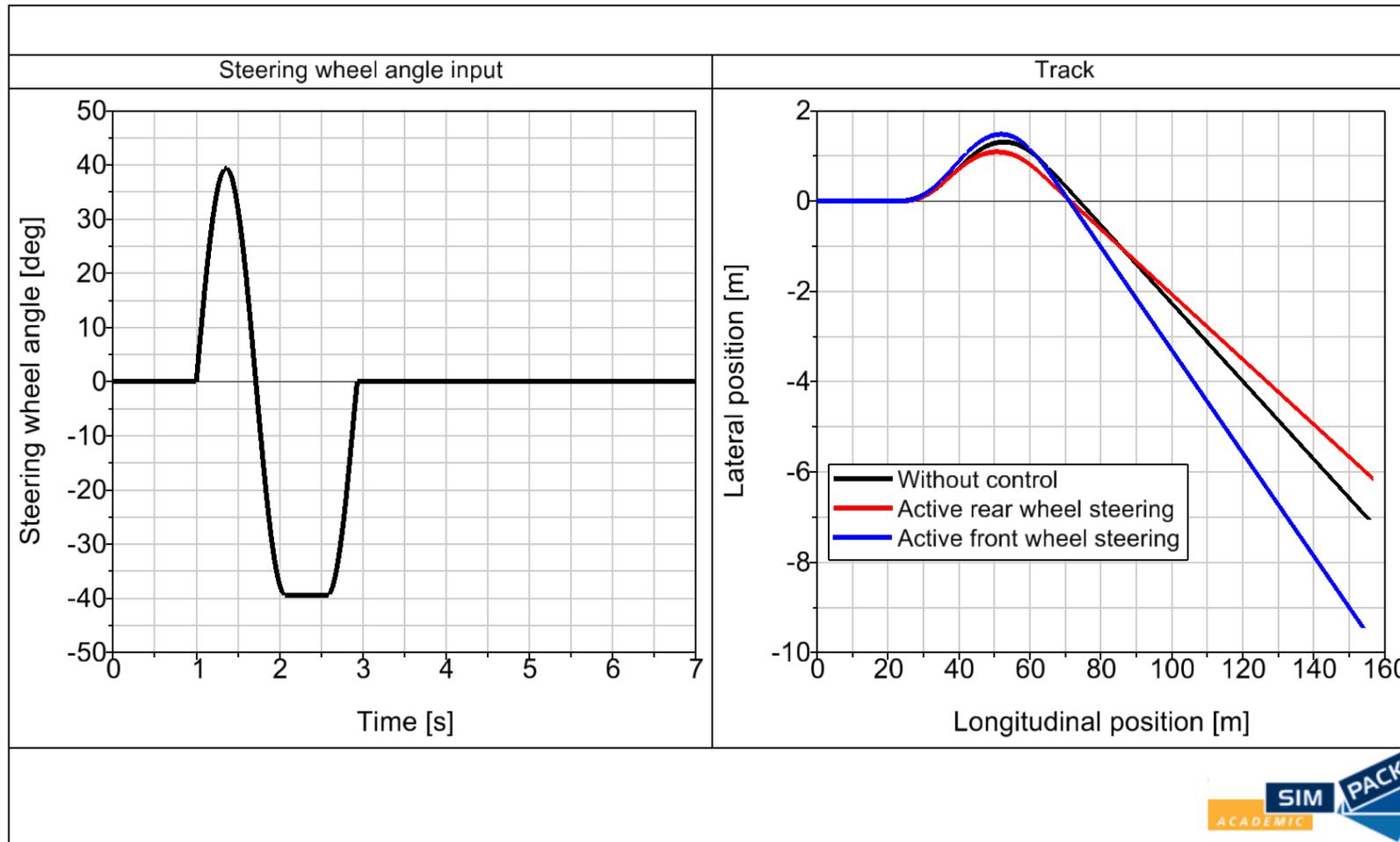
Driver	objective, no driver influence
Velocity	80 km/h
Steering wheel angle input	single sine of 0.7 Hz with dwell of 500 ms after $\frac{3}{4}$ of period, steady-state lateral acceleration of amplitude is 0.4 g
Road surface	dry, $\mu = 0.9$



Sine with dwell: Simulation results

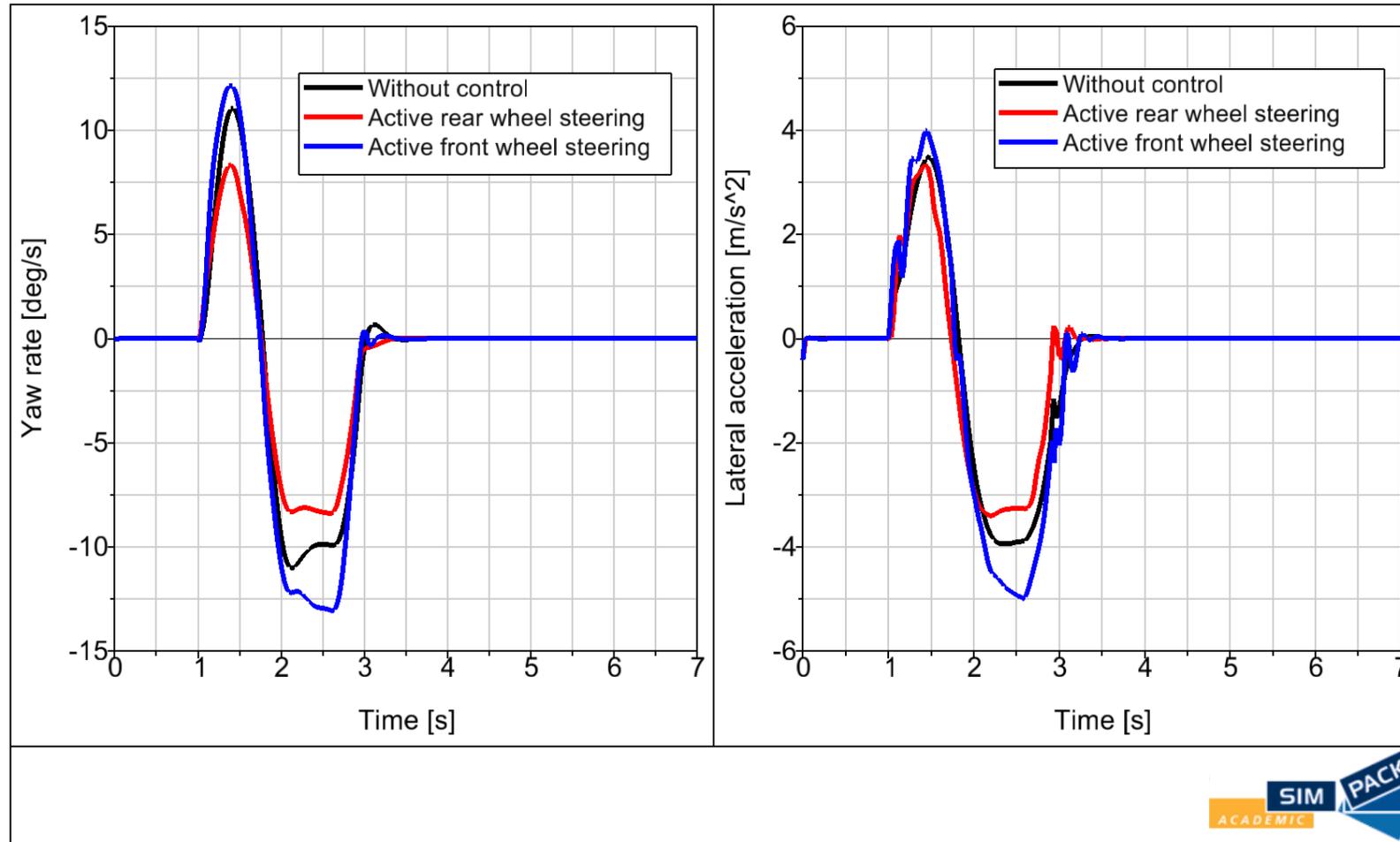


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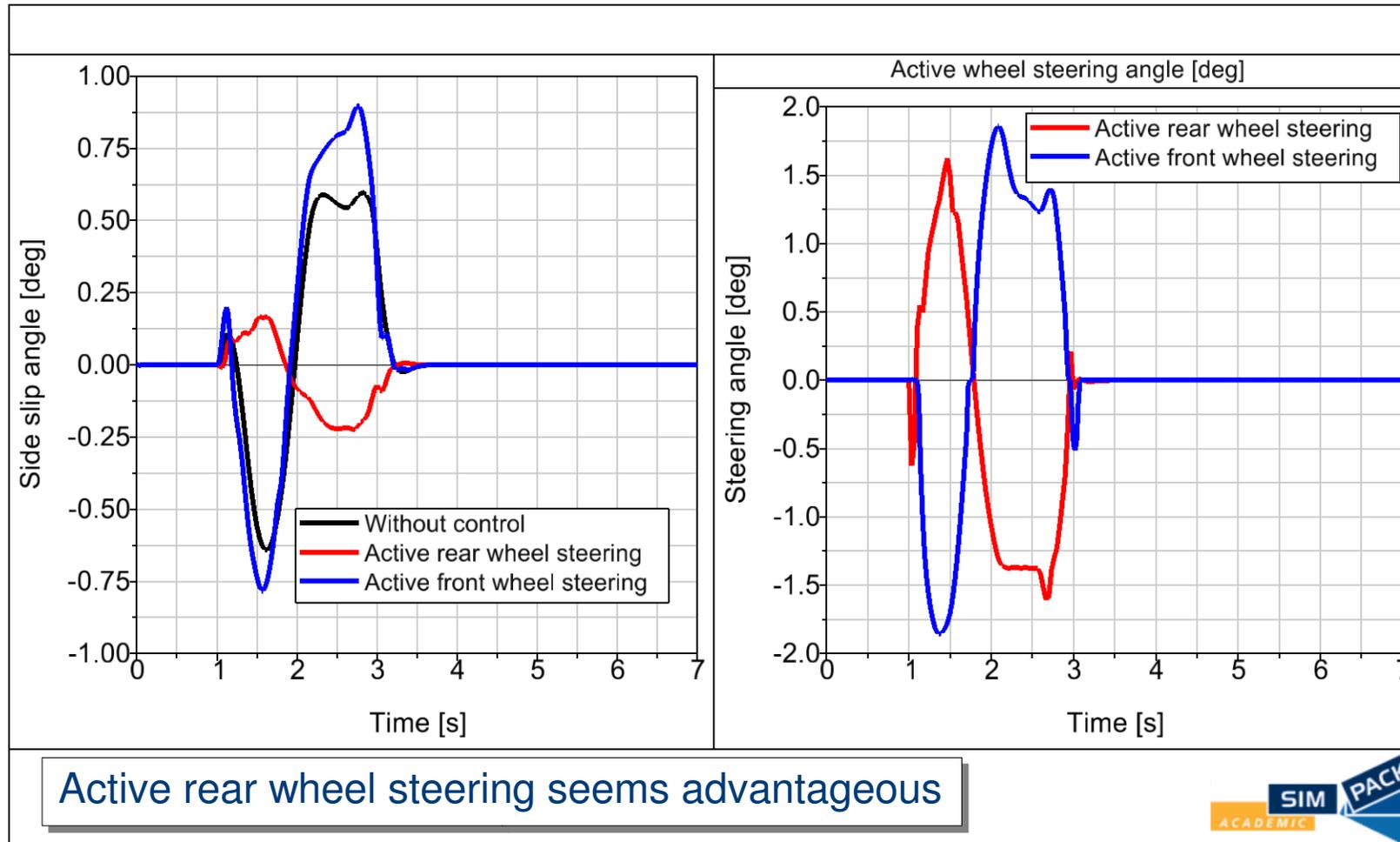
Sine with dwell: Simulation results

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Sine with dwell: Simulation results

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Sine with dwell on slippery road

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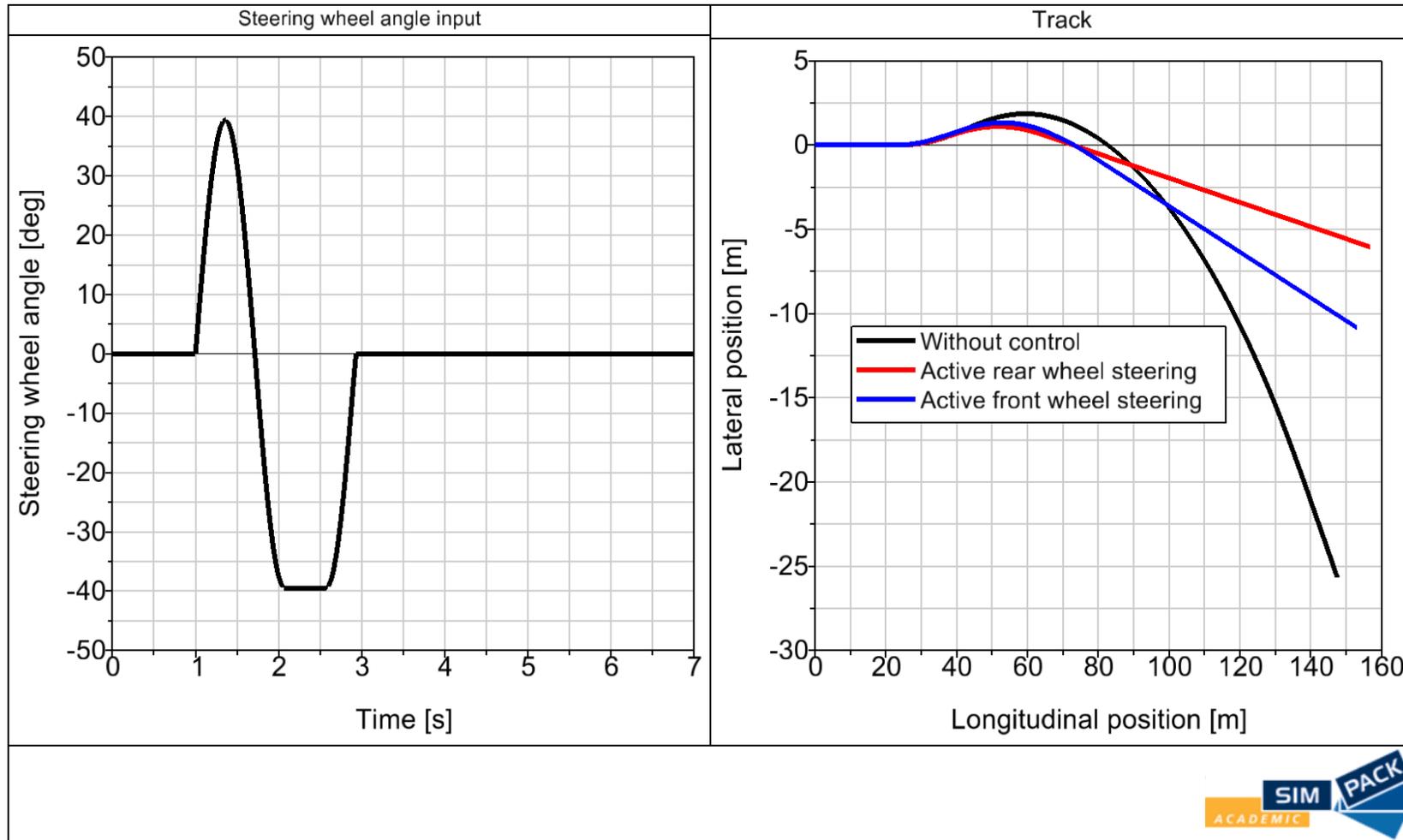
Driver	objective, no driver influence
Velocity	80 km/h
Steering wheel angle input	single sine of 0.7 Hz with dwell of 500 ms after $\frac{3}{4}$ of period, steady-state lateral acceleration of amplitude is 0.4 g (for vehicle without control)
Road surface	slippery, $\mu = 0.35$



Sine with dwell on low μ : Simulation results



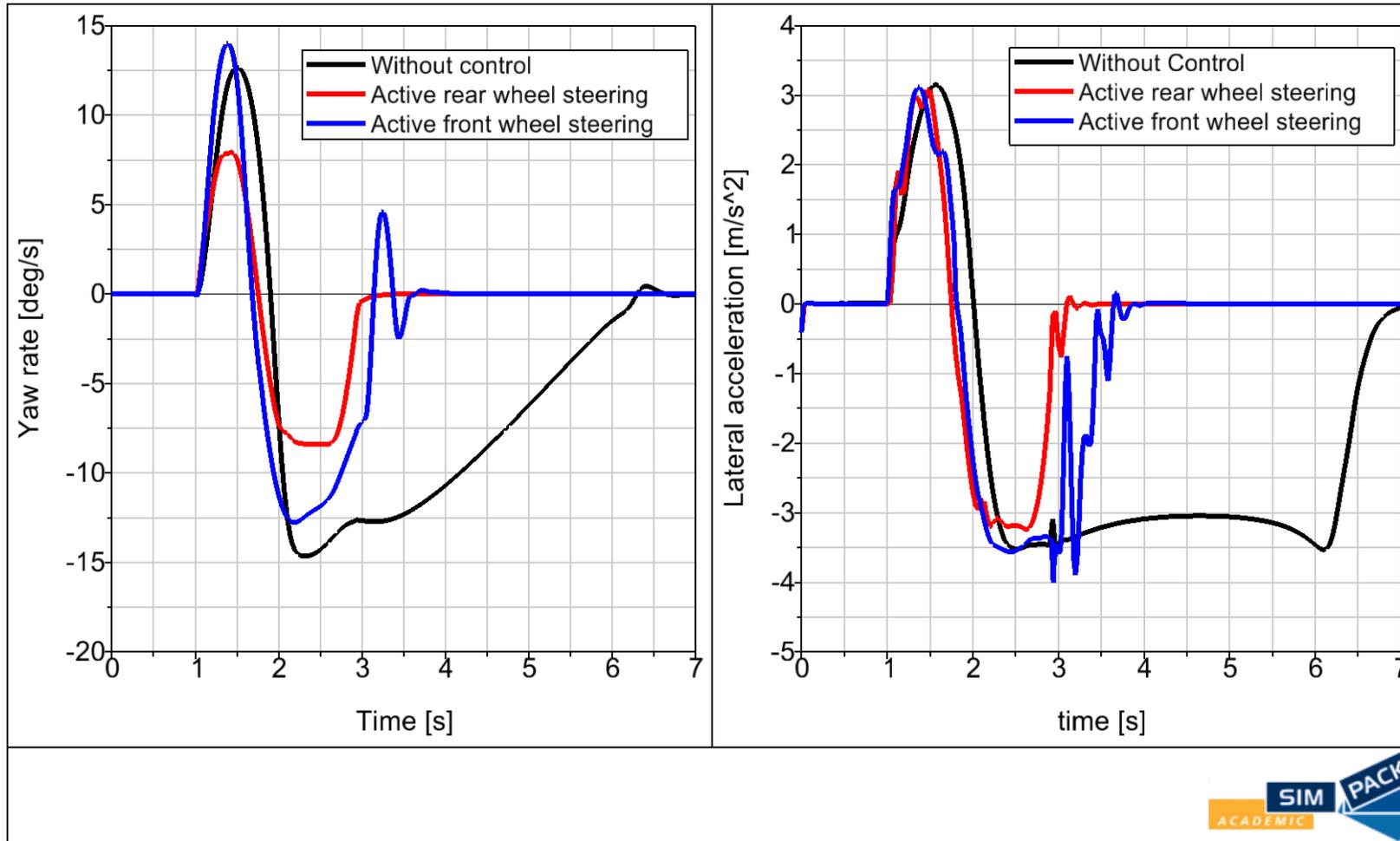
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Sine with dwell on low μ : Simulation results



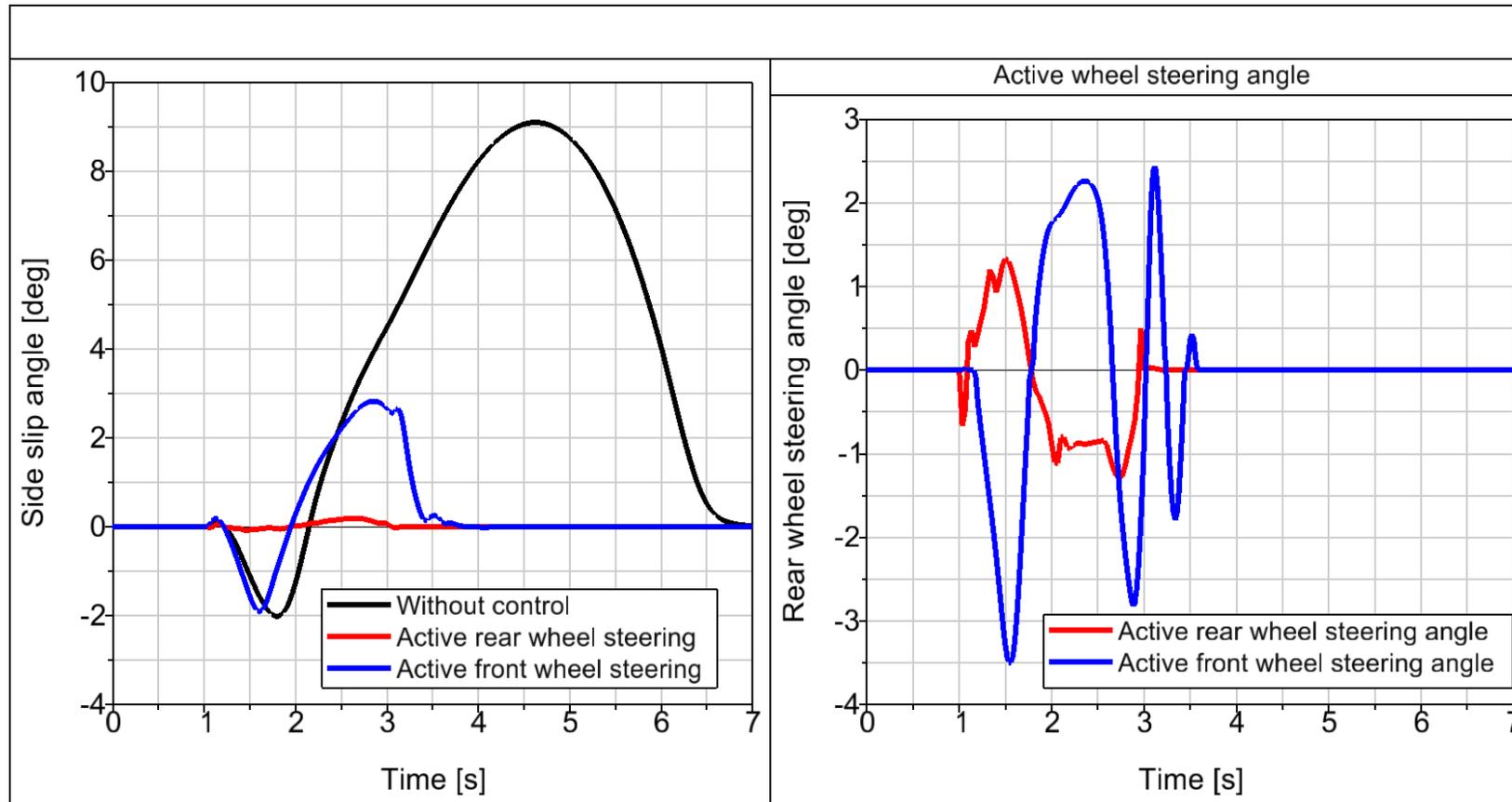
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Sine with dwell on low μ : Simulation results



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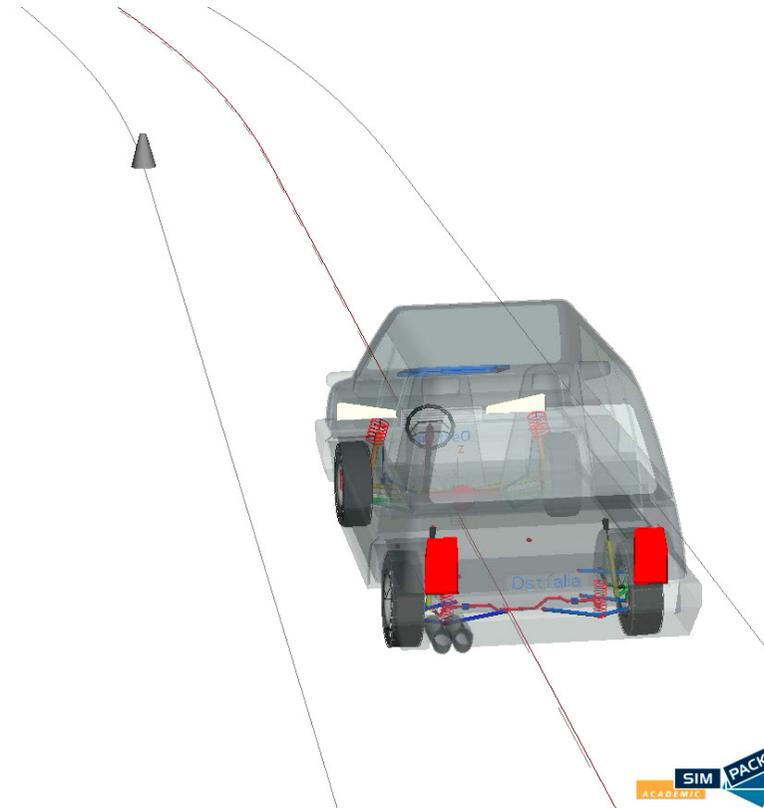
Active steering makes this maneuver driveable,
rear wheel steering is most effective



Maneuver slalom

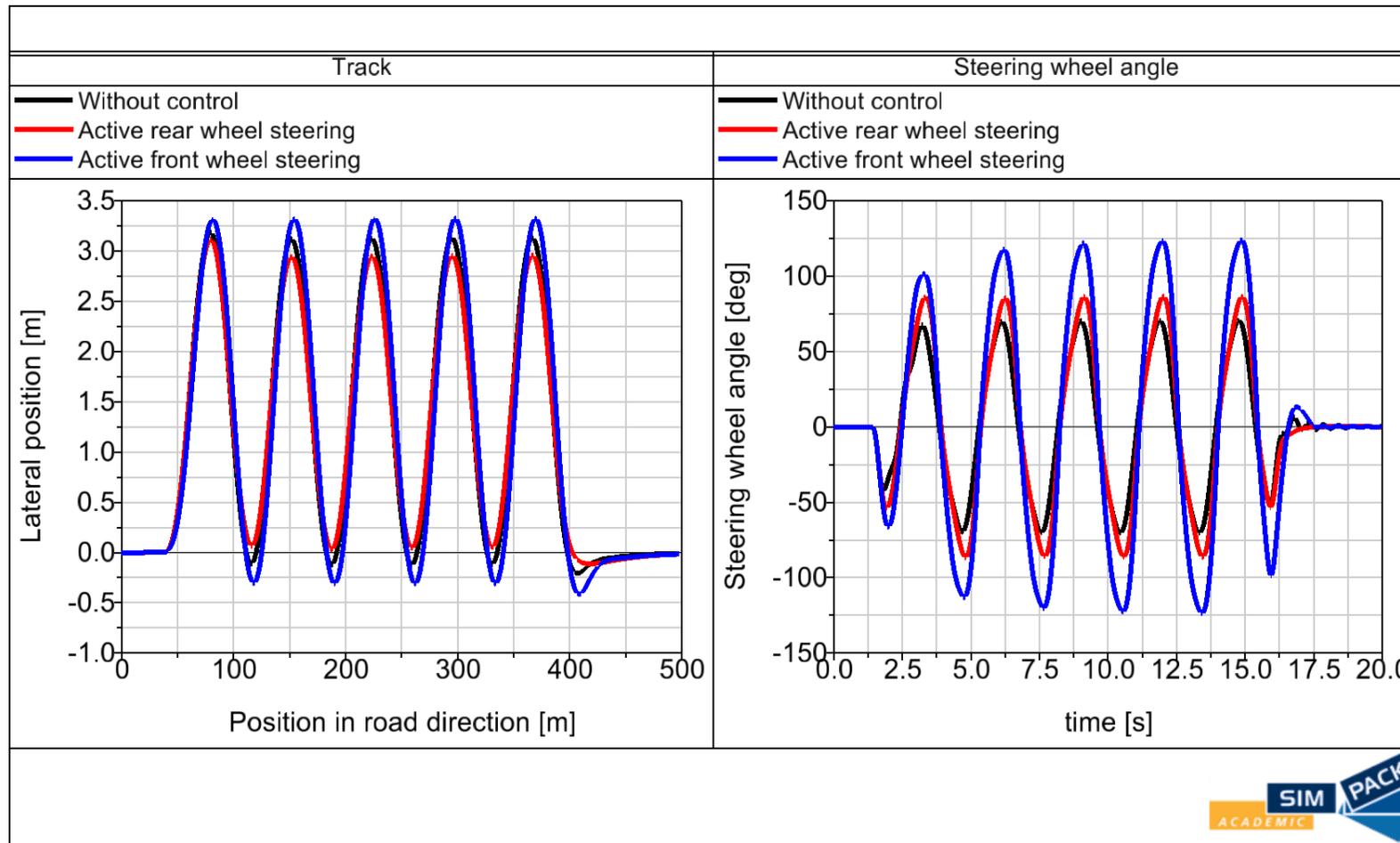
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driver	Simpack driver model, driver influence
velocity	90 km/h
front wheel steering angle	closed loop, by driver
road surface	dry, $\mu = 0.9$



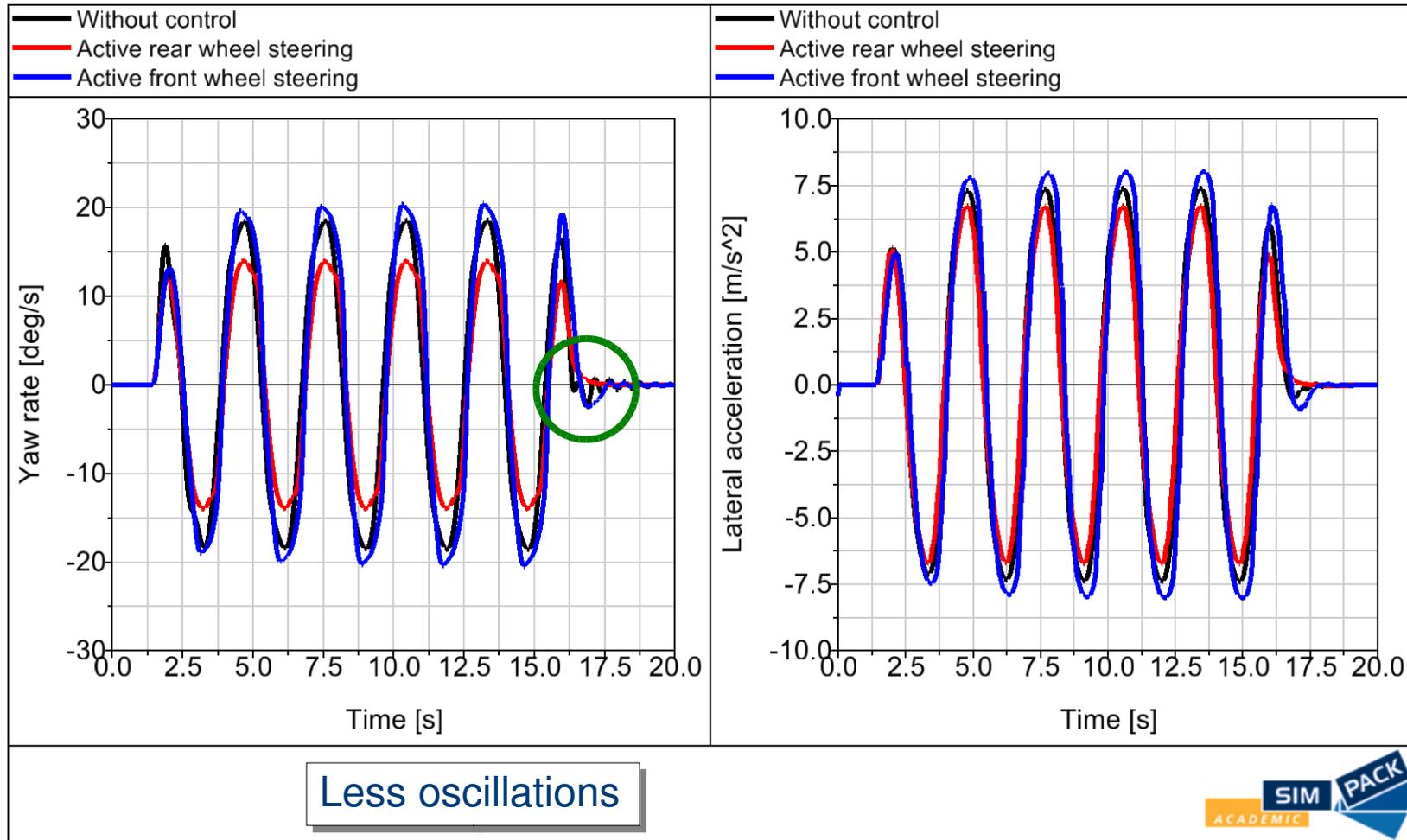
Slalom: Simulation results

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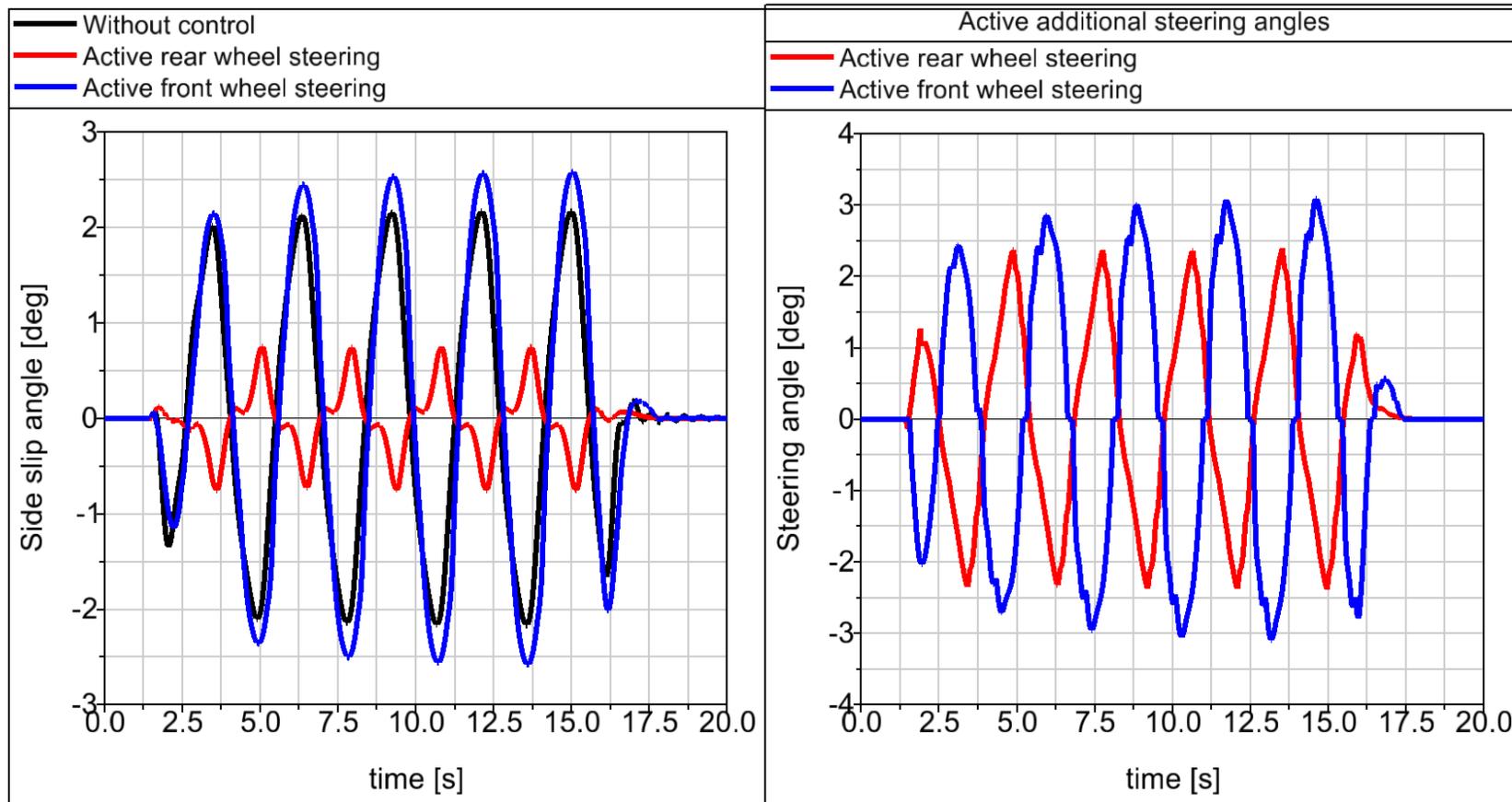
Slalom: Simulation results

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Slalom: Simulation results

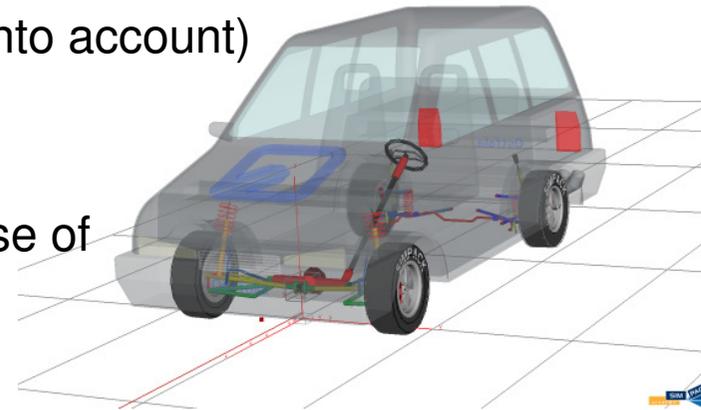
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Rear wheel steering is advantageous



- Validated mbs vehicle model as a basis
- Simple implementation of active steering systems by additional dofs: rear wheel steering, front wheel steering
- Co-Simulation of Simpack and Matlab/Simulink® for integration of control systems
- Systems work effectively, effects on vehicle dynamics can be studied, active rear wheel steering seems more powerful
- Optimization of both systems still needed (optimize control parameters, take side slip limit and wheel slip into account)
- Mechanical design of rear wheel steering and implementation of an actor model
- Implementation of a steering actor model in case of front wheel steering



Acknowledgment

The author would like to thank Yangfang Yu for doing a lot of excellent modeling and simulation work.